





EXPERIMENTAL INVESTIGATION OF HIGH FREQUENCY COMBUSTION INSTABILITY IN CRYOGENIC OXYGEN-HYDROGEN ROCKET ENGINES

Justin S. Hardi

Experimental Investigation of High Frequency Combustion Instability in Cryogenic Oxygen-Hydrogen Rocket Engines

Justin S. Hardi

School of Mechanical Engineering
The University of Adelaide
South Australia 5005
Australia

A thesis submitted in fulfilment of the requirements for the degree of Ph.D in Aerospace Engineering in June 2012

Contents

Cc	ontents	S		ii
Lis	st of fi	gures		vi
Lis	st of ta	bles		x
GI	ossary	·		xi
Αk	ostract			xiii
De	eclarat	on of original	ity	xv
		J	nd disclaimer	
1.		-		
2.	Вас	kground		3
	2.1	Launch vehicles		3
	2.2	Rocket propulsio	n	4
	2.3	Liquid propellant	rocket engines	6
	2.3		opellant rocket engine performance	
	2.3	4	ppellants	
	2.3	,	/pes	
	2.3	•	nts	
	2.4		n propellant combination	
	2.4 2.4		n fuelygen oxidiser	
	2.4	1	ical conditions	
	2.5		mber processes	
	2.5		it injection	
	2.5		on of liquid propellants	
	2.5		ry atomisation	
	2.5 2.5		tion	
			ion	
	2.6		ability	
	2.6 2.6		rising combustion instabilityuency combustion instability	
	2.6		nechanisms of instabilities	
	2.6		g combustion instability	
3.	Lite	rature survey		27
	3.1	Investigations up	to 1972	27
	3.2	Investigations fro	m 1972 to 1995	36
	3.3	ū	search	
	3.4	• .	oility research	
	3.4		ting flows	
	3.4		<u> </u>	45

	3.5	Sumn	nary	51
4.	Cor	mbust	tor development	53
	4.1	Expe	rimental combustor review	53
	4.1	•	Historical overview	
	4.	1.2	CRC	
		1.3	MIC and VHAM	
		1.4	Pennsylvania State University rectangular combustor	
		1.5	Purdue University rectangular combustor	
	4.′	1.6	Summary	60
	4.2	New	combustor specifications	
	4.2		Operating conditions	
		2.2	Test facility	
	4.2	2.3	Injector	
	4.3		eptual design	
	4.3		Concept 1: High pressure CRC	
		3.2	Concept 2: Rectangular chamber	
		3.3	Concept 3: Excitation segment for BKB	
		3.4 3.5	Concept 4: Ring resonator segment for BKB Concept 5: Twin resonator segment for BKB	
		3.6	Concept selection	
			•	
	4.4		rectangular combustor: BKH	
	4.4	4.1 4.2	BKH concept overview Combustion chamber acoustics	
		4.2 4.3	Primary injector	
		4.4	Secondary injection	
		4.5	Diagnostics	
	4.4	4.6	Optical access	
	4.4	4.7	Excitation system	76
5.	Exp		ental techniques	
	5.1		operations	
		1.1	Test facility	
		1.2	Test campaigns	
		1.3	Hardware integration	
		1.4 1.5	Test runs Test sequences	
			•	
	5.2	Diagr	nostics and data acquisition	85
	5.3	Optic	al diagnostics	
		3.1	OH* chemiluminescence imaging	
		3.2	Shadowgraph imaging	
	5.3	3.3	OH* chemiluminescence recording with photomultipliers	88
	5.4	Camp	paigns 1 and 2: initial hardware testing	
	5.4		Test type 1; clean configuration	
		4.2	Test type 2; clean configuration with optics	
		4.3	Test type 3; with excitation and optics	
	5.5		paigns 3 and 4: excitation and optics with ambient hydrogen	
	5.5		Test type 4; with excitation	
	5.5	5.2	Test type 5; with excitation and optics	
	5.6	Camp	paign 5: excitation and optics with cryogenic hydrogen	
	5.6		Test type 6; cold flow with excitation	
	5.6	6.2	Test type 7; with excitation and optics	
	5.7	Sumn	nary of achieved operating conditions	102
_	_	. .		
h	Δcc	nietic	characterisation	103

	C.1	Round	d nozzle	205
Αį	•	dix C.	Modified secondary nozzle	
			•	
Αļ	open B.1	dix B.	BKH dimensionsustor drawings	
	A.5		facture feasibility study	
	A.4		condensation	
	A.3		ndary injection	
	A.2		al flow	
•	. A.1		resonator segment geometry	
Αį	pen	dix A.	Twin resonator segment design study	189
11	. Re	eferenc	es	179
10). Oı	utlook.		177
9.	Co	onclusi	ons	175
	8.6	Sumn	nary	173
	8.5	Secor	ndary atomisation	170
	8.4	Intact	core length measurements	164
	8.3	Dynar	mic response to transverse excitation	161
	8.2	Oxyge	en core structure	155
	8.1	Revie	w of oxygen core studies	153
8.	O	xygen o	core response	153
	7.8	Sumn	nary	150
	7.7		multiplier response measurements	
	7.6	•	mic response to longitudinal excitation	
	7.5	•	mic response to transverse excitation	
	7.4	-	mic OH* emission response	
	7.3	Flame	e displacement	135
	7.2	Flame	e structure	131
	7.1	Revie	w of flame response studies	129
7.	Fl	ame res	sponse	129
	6.7	Sumn	nary	128
	6.6	Injecti	on coupling	124
	6.5	Comb	ustion response	121
		6.4.2 6.4.3	Low frequency instability Excitation amplitude	
		6.4.1	Spectrum characterisation	
	6.4	Acous	stic excitation	114
	6.3	Syste	m modification: acoustic baffle	110
	6.2	Spect	rum characterisation	105
	6.1	Finite	element acoustic model	103

C.2	Double sine nozzle	206
∆nnandi	lix D. List of articles resulting from this work	209
	Journal articles	
	Conference papers	

List of figures

Figure 2.1: Heavy launch vehicles using LPREs; (from left to right) Ariane 5 (Arianespace 2012), Space Shutt 2007), Soyuz (Arianespace 2012), and Delta IV (Boeing 2007).	
Figure 2.2: Schematics of liquid, solid and hybrid rocket propulsion systems (Image credit: Andrew Sysouphat 2005	5)5
Figure 2.3: Ariane 5 launch vehicle highlighting the main components (modified from DKimages 2007)	
Figure 2.4: Schematic diagram of the main components of a liquid rocket (Sutton & Biblarz 2001, p.8)	
Figure 2.5: Schematic diagrams of several liquid rocket injector types (Sutton & Biblarz 2001, p.274)	
Figure 2.6: The injector assembly of the J-2 engine (left) (Dykema 1972, p.360), and an illustration of a simple she injector with no recess (right).	er coaxial 10
Figure 2.7: Pressure balance on a typical thrust chamber (Sutton & Biblarz 2001, p.33).	
Figure 2.8: Phase diagram indicating transcritical injection of oxygen, c_p values from Younglove (1982)	13
Figure 2.9: Critical mixing lines for three binary systems (Mayer & Smith 2004, p.8).	14
Figure 2.10: Comparison of coaxial injection at subcritical and supercritical pressures (Mayer & Tamura 1996, p.114	46)15
Figure 2.11: Typical traces of chamber pressure with time for smooth and rough combustion (Sutton & Biblarz 200	01, p.349).
Figure 2.12: Characteristics of transverse modes.	19
Figure 2.13: Cutaway sketch of a thrust chamber showing the injector-face baffle (Harrje & Reardon 1972, p.157)	23
Figure 3.1: Cutaway sketch of the variable-angle sector motor (Crocco, Harrje & Reardon 1962, p.368)	
Figure 3.2: Droplet stream response to external acoustic forcing for three parallel jets (images of better quality ur (Miesse 1955, p.527).	navailable)
Figure 3.3: Oxygen jet length reduction during transverse mode acoustic instability (Heidmann 1965b, p.10)	
Figure 3.4: Response factor curve for n-heptane based on vaporisation parameters (Heidmann & Wieber 1966a, p.8 Figure 3.5: Response curves for heptane and oxygen (Heidmann & Wieber 1966b, p.17).	8) 33
Figure 3.6: Flame and flow field imaging of the near injector region of a reacting flow of LOx/H ₂ at 45 bar chamber	
(modified from Mayer et al. 1996).	
Figure 3.7: Comparison of back-lit shadowgraph imaging of the flow field for (a) subcritical and (b) supercritical pressures (modified from Mayer et al. 1996).	l chamber
Figure 3.8: Interaction of acoustic waves with a single LN ₂ jet injected into GN ₂ under subcritical conditions (Chehr	
2003, p.19)	42
Figure 3.9: Interaction of acoustic waves with a coaxial jet of LN ₂ /GN ₂ under supercritical conditions (Chehroudi e	tal 2003
p.26)	43
Figure 3.10: Consecutive frames from high-speed shadowgraph imaging of acoustic forcing of a coaxial nitrogen	
subcritical, near-, and supercritical conditions (Davis & Chehroudi 2006, p.5)	
Figure 3.11: V-profile pressure ramping test (Smith et al. 2004, p.11).	
Figure 3.12: Instantaneous and time- averaged OH* emission images (in false colour) from the MIC, without (left co	lumn) and
with (right column) 1T mode excitation (Richecoeur 2006, p.78)	
Figure 3.13: Configuration of the multi-element rectangular combustor (top, cross-sectional view) with the first ar	
mode shapes superimposed (Marshall et al. 2006a, p.3).	
Figure 3.14: Purdue University rectangular combustor with central swirl coaxial study element (Wierman, Nugent &	
2011, p.3)	
Figure 4.1: Streak photography of a rotating 1T mode instability (Tischler & Male 1956).	54
Figure 4.2: Working principle of small rocket combustor with intermittant nozzle modulation (Lecourt & Foucaud 1	
Figure 4.3: CRC combustor for HF research (Knapp, Farago & Oschwald 2007, p.3)	56
Figure 4.4: Pressure fields in the DLR combustor with the secondary nozzle in the 180° position (left) and the 90	
(right) (Knapp, Farago & Oschwald 2007, p.3).	
Figure 4.5: Illustration of the MIC configuration with three injection elements (left, middle), and a photograph or element version of the injector (right) (modified from Richecoeur 2006).	of the five-
Figure 4.6: Illustration of the MIC equipped with the VHAM (left) (Méry et al. 2008), and a numerically calculated	
pressure distribution (right) (Richecoeur 2006, p.246)	59
Figure 4.7: Penta-injector pattern and relative acoustic field orientation.	63
Figure 4.8 High pressure CRC concept (internal geometry)	63
Figure 4.9: Rectangular combustor concept (internal geometry)	
Figure 4.10: First three acoustic mode shapes for the MIC illustrating the influence of the secondary nozzle	
symmetry (Richecoeur 2006, p.57)	
Figure 4.11: Experimental combustor BKB (Suslov et al. 2005, p.3)	
Figure 4.12: BKB with excitation segment concept (internal geometry).	
Figure 4.13: BKB with ring resonator concept (internal geometry).	

Figure 4.14: Numerically calculated BKB-ring resonator chamber resonance modes	68
Figure 4.15: Twin resonator segment concept (internal geometry)	68
Figure 4.16: Twin resonator segment resonance modes of interest	
Figure 4.17: BKH combustor concept.	
Figure 4.18: Internal volume of the BKH combustion chamber.	
Figure 4.19: Pressure distributions for the resonance modes of a simple rectangular volume as listed in Table 4	
Figure 4.20: BKH Penta-injector pattern dimensions	
Figure 4.21: Injector faceplate showing secondary hydrogen injection arrays, and the desired influence on the flow field	
Figure 4.22: Dynamic pressure sensor locations and model names in BKH	
Figure 4.23: Optical access windows and dummy windows	
Figure 4.24: Modal analysis results showing the influence of secondary nozzle length on the 1T mode structure.	
numerical mode calculations were conducted in FlexPDE using a sound speed of 1712 m/s. The primary	
secondary nozzle exit sizes have been scaled for two-dimensionality.	
Figure 4.25: Photographs of the excitation system installed on BKH.	
Figure 4.26: The excitation system on BKH with housing installed.	
Figure 5.1: European Test Facility 'P8' for cryogenic rocket engine research	
Figure 5.2 BKH integration with the P8 test facility	
Figure 5.3: Photographs of the test cell during a BKH test run, taken from the D68 control building	
Figure 5.4: Emission spectrum from a LOx/H ₂ sub-scale combustor	
Figure 5.5: BKH configuration for test type 1; clean configuration	
Figure 5.6: Example test sequence for test type 1; staged ROF.	
Figure 5.7: BKH configuration for test type 2; clean configuration with optics.	
Figure 5.8: Initial optical setup for campaigns 1 and 2	
Figure 5.9: Example test sequence for test type 2; staged ROF with optics.	
Figure 5.10: Example shadowgraph images from test type 2, for a 40 bar operating condition with ROF = 2 (left), and	
ROF = 6 (right)	
Figure 5.11: BKH configuration for test type 3; with excitation and optics.	
Figure 5.12: Exciter wheel modification.	
Figure 5.13: Example test sequence for test type 3; uncontrolled excitation ramp with optics	
Figure 5.14: Example shadowgraph images from off-resonance conditions in test type 3, at 50 bar with ROF = 6 (left), an	
bar with ROF = 6 (right).	
Figure 5.15: Example instantaneous raw OH* images from test type 3, taken from off-resonance excitation at t = +4 s	
and 1T mode excitation at t = +5.3 s (b).	
Figure 5.16: Video frames during sequence failure, and resulting hardware damage	
Figure 5.17: Example test sequence for test type 4; controlled excitation ramp Figure 5.18: Modified optical setup	
Figure 5.19: Photos of the modified optical setup.	
Figure 5.20: Example shadowgraph images from a test at 40 bar with GH ₂ (a), and a test at 60 bar with GH ₂ (b)	
Figure 5.20. Example test sequence for test type 5; with excitation and optics	
Figure 5.21: Example test sequence for test type 3, with excitation and optics Figure 5.22: Instantaneous raw OH* images from the test in Figure 5.21 during off-resonance (a) and 1T-mode excitation	
rigure 3.22. Instantaneous raw Orr innages nom the test in rigure 3.21 during on-resonance (a) and 11-mode excitation	. ,
Figure 5.23: Example spectrogram from a photomultiplier.	
Figure 5.24: Example shadowgraph images from a test at 40 bar with LH ₂ (a), and at 60 bar with LH ₂ (b)	
Figure 5.25: Sensing areas of the photomultipliers for test type 7	
Figure 5.26: Achieved operating conditions of BKH.	
Figure 6.1: Finite element model of BKH showing (a) the fluid property groups (for the configuration with secondary noz	
and (b) the meshed model (without secondary nozzle).	
Figure 6.2: PSD spectrum of dynamic pressure signals from <i>PCCdyn2</i> (a), and from <i>PIHdyn</i> (b). <i>PIHdyn</i> is shown	
indicated mode frequencies as calculated using the FE model.	
Figure 6.3: Example FE-calculated pressure distributions of some secondary H ₂ manifold acoustic modes	
Figure 6.4: PSD of <i>PCCdyn</i> 2 with analytical and FE calculated mode frequencies indicated (a), and with actual char	
resonance modes identified as 'selected' (b).	
Figure 6.5: Mode identification by sensor phase analysis for the 1L mode at 3200 Hz (a), 1T mode at 4370 Hz (b), and	
mode at 5370 Hz (c)	
Figure 6.6: PSD of <i>PCCdyn2</i> with FE calculated mode frequencies indicated for both ideal sound speed and sound speed.	
corrected for c* combustion efficiency.	
Figure 6.7: Design of the acoustic baffle for the secondary H ₂ manifold. Also shown is the geometry of the FE model with	
baffle included	
Figure 6.8: Results with the acoustic baffle installed in the secondary H_2 manifold; (a) PSD of <i>PIHdyn</i> without baffle (repe	
here for convenience), (b) PSD of <i>PIHdyn</i> with baffle, and (c,d) the corresponding PSD of <i>PCCdyn1</i>	
Figure 6.9: Power spectra comparing primary combustion chamber modes with and without secondary nozzle installed	

Figure 6.10: FE-calculated pressure distributions for the 1T mode; (a) without, and (b) with the secondary nozzle	
Figure 6.11: Mode identification by sensor phase analysis with on-resonance excitation for the 1L mode (a), 1T and 1L1T (c)	mode (b)
Figure 6.12: Spectrogram of a type 4 test; steady-state conditions with a controlled excitation ramp from 1000 to	6000 Hz
Figure 6.13: Spectrogram of Figure 6.12, viewed up to 40,000 Hz, with excitation signal overtones indicated	
Figure 6.14: Spectrogram from a 60 bar test illustrating transitioning LF chugging during transverse mode excitation	118
Figure 6.15: Dynamic pressure signal during ramped excitation of the 1L, 1T and 1L1T modes. The calculated	dacoustic
pressure amplitude is overlayed (red line). The ramped excitation frequency (blue line) is also overlayed for in	formation
Figure 6.16: Spectrogram of the PCCdyn2 signal from an early test with uncontrolled excitation ramp	
Figure 6.17: Progression of acoustic pressure amplitude during 1T mode excitation for a cold-flow test without co (a), and a hot-fire test at 60 bar with GH ₂ (b)	122
Figure 6.18: Spectrogram showing ramped excitation of the 1T and 1L1T modes for a 40 bar test with LH2	
Figure 6.19: Combustion chamber and injection manifold acoustic spectra during peak 1T-mode resonance ampli the 40 bar test with LH ₂ in Figure 6.18	
Figure 6.20: Combustion chamber and injection manifold acoustic spectra during off-resonance excitation from the	he 40 ba
test with LH ₂ in Figure 6.18	125
Figure 6.21: FE model results for acoustic modes of the H ₂ injector (left column) and the LOx injector (right column).	
Figure 7.1: Instantaneous OH* emission image, shown in false-colour (a), and corresponding shadowgraph image (off-resonance conditions	
Figure 7.2: Time-averaged shadowgraph (a) and OH* emission (b) images during off-resonance conditions in a 6	
with GH ₂	133
Figure 7.3: Time-averaged OH* emission images during off-resonance conditions in 40 bar, LH ₂ test A (a), and in 40 test B (b)	
test B (b).	
Figure 7.4: Time-averaged shadowgraph (a) and OH* emission (b) images during 1T mode excitation with $p'/P_{cc} = 7$	
Figure 7.5: Projected cross-section of the flames from the 40 bar test with LH ₂ , case A	
Figure 7.7: Example sequence of images used to measure transverse (i.e. vertical) displacement of the flame of mode excitation. The raw OH* image (upper row) and its converted binary counterpart (lower row) are shown.	
Figure 7.8: Comparison of transverse flame displacement measurements and acoustic particle displacement signals	
Figure 7.9: Spectrogram of mean OH* emission from high-speed imaging at 40 bar with LH ₂ , case B	
Figure 7.10: Spectrogram of mean OH* emission from high-speed imaging at 40 bar with GH ₂	
Figure 7.11: Spectrogram of mean OH* emission from high-speed imaging at 40 bar with GH ₂	
Figure 7.12: Spectrogram of photomultiplier signal at 40 bar with GH ₂ .	
Figure 7.13: Spectrogram of photomultiplier signal at 40 bar with GH ₂ .	
Figure 7.14: Reconstructed acoustic pressure and velocity distributions of the 1T mode used for the calculation of	
indices; (a) at the point of peak acoustic pressure for PCCdyn2 (a), and one-quarter of a cycle later at the point	nt of peal
velocity amplitude (b)	
Figure 7.15: Response of the flame to 1T mode resonance comparing time-averaged distributions of the raw OH* in the pressure based Rayleigh index (b), the velocity based Rayleigh index (c), acoustic pressure phase (d), and	
velocity phase (e)	
Figure 7.16: Sequence of raw OH* images (upper row) and band-pass filtered emission distribution (lower row) is	•
how transverse (up and down) convective motion results in artefact signals in band-pass images. Two exam	
sequences are given from excitation of the 1T mode at 4350 Hz	145
Figure 7.17: Reconstructed acoustic pressure and velocity distributions of the 1L mode used for the calculation of	
indices; at the point of peak acoustic pressure in the window (a), and one-quarter of a cycle later at the poir velocity amplitude (b). The velocity antinode is located downstream of the window.	
Figure 7.18: Response of the flame to 1L mode resonance comparing time-averaged distributions of the raw OH* in	
the pressure-based Rayleigh index (b), the velocity-based Rayleigh index (c), acoustic pressure phase	e (d), and
acoustic velocity phase (e)	148
Figure 7.19: Response factor distribution for coupling of OH* emission with acoustic pressure during 1L-mode restests at 60 bar with GH ₂ , cases A (a) and B (b).	
Figure 7.20: Response factors for coupling of OH* emission with acoustic pressure during 1L-mode resonance	
Figure 8.1: Example instantaneous shadowgraph image (a) and corresponding instantaneous OH* emission image,	
false colour (b), for a 60 bar test with GH ₂	
Figure 8.2: Natural LOx core breakup behaviour at 60 bar with GH ₂	
Figure 8.3: Map of shear-coaxial breakup regimes defined by Chigier and Reitz (1995)	
Figure 8.4: Coaxial air and liquid injection with breakup in the fibre-type regime (Chiqier & Reitz 1995, p.120)	

Figure 8.5: Comparison of shadowgraph images for subcritical (40 bar) and supercritical (60 bar) chamber pressure	
tests at 40 bar with GH ₂ (a), 60 bar with GH ₂ (b), 40 bar with LH ₂ (c), and 60 bar with LH ₂ (d)	
Figure 8.6: Critical mixing lines of common binary systems (Mayer & Smith 2004, p.8).	
Figure 8.7: Surface tension of the oxygen/hydrogen binary system (Mayer & Smith 2004, p.8).	
Figure 8.8: Time-averaged shadowgraph (upper row) and OH* emission images (lower row) during off-resonance e (a), and 1T-mode excitation with $p'/P_{cc} = 7.4\%$ (b)	162
Figure 8.9: Sequential shadowgraph images from a 60 bar test with GH ₂ , recorded at 20,000 fps during 1T mode e	xcitation
with $p'/P_{cc} = 7.4\%$	163
Figure 8.10: Major steps in the semi-automated core detection routine; the binary image created following pre-pro	
with the user-specified analysis area (a), the intact core centreline (b), and the centerline overlaid on the raw in	• ,
Figure 8.11: Acoustic pressure signals and shadowgraph recording durations for 60 bar, GH ₂ case A (a), and case C shadowgraph recording rates of 7000 fps and 20,000 fps, respectively.	. ,
Figure 8.12: Frame-by-frame measurements of the intact LOx core length from 5-ms duration (100-frame) samples	
case C test at 60 bar with GH ₂ . The first sample is from the beginning of the shadowgraph recording in	
Figure 8.13: Normalised intact core length (L/D) plotted against relative acoustic pressure amplitude (p'/P_{cc})	
Figure 8.14: Normalised intact core length (L/D) plotted against the ratio of transverse-acoustic to H ₂ -injection mo	
flux	
Figure 8.15: Normalised intact core length (<i>L/D</i>) plotted against transverse acoustic Weber number	
Figure 8.18 Comparison of break-up regime transitions for LOx in dry air and helium under 30 bar (Vieille, Char	
Gokalp 1999)	
Figure 8.19 Experimental data and the corresponding transition criteria for liquid oxygen droplet breakup regimes Chauveau & Gokalp 1999)	
Chauveau & Gokaip 1999)	173
Figure A.1: Twin resonator segment concept with square resonator (internal geometry)	180
Figure A.2: Concepts for internal geometry at the resonator chamber intersection	
Figure A.3: Dimensions of twin resonator chamber internal geometry.	
Figure A.4: Estimated flow pattern near the resonator-chamber intersection.	
Figure A.5: Meshed model of the TRS for CFD analysis.	
Figure A.6: Velocity field results for CFD Case 1	
Figure A.7: Velocity field results for CFD Case 2	
Figure A.8: Velocity field results for CFD Case 3	
Figure A.9: Individual jet streamlines for CFD Case 3.	
Figure A.10: Concept for secondary hydrogen injection.	
Figure A.11: Secondary injection CFD model geometry	
Figure A.12: CFD streamline results comparison for TRS secondary injection.	
Figure A.13: CFD calculated gas temperature distribution for the TRS with secondary H2 injection	
Figure A.14: Acoustic mode comparison for TRS with and without secondary H2	
Figure A.15: TRS heat load with and without secondary H ₂ injection	
Figure A.16: Acoustic mode shapes with nitrogen injection	
Figure A.17: Example numerical acoustic pressure distributions for the TRS, with and without pooled water condensa	te199
Figure B.1: Overview of the internal volumes of BKH	201
Figure B.2: Dimensions of the internal volumes of BKH.	202
Figure B.3: Detailed BKH injector dimensions.	
Figure B.4: Locations of sensors in BKH.	
Figure C.1: A photograph of the round secondary nozzle (a), and the corresponding excitation profile (b)	
Figure C.2: A photograph of the secondary nozzle with double sine profile (a), and the corresponding excitation pr	ofile (b).
Figure C.3: Comparison of acoustic pressure spectra in the combustion chamber for excitation with the round a	
profiled secondary nozzles. Spectra are shown for stationary, off-resonance excitation (a), and for ramp	
resonance excitation (b)	
\-\ \-\ \-\ \-\ \-\ \-\ \-\ \-\ \-\ \-\	

List of tables

Table 1: Typical specific impulse for chemical rocket types.	8
Table 2: Specific impulse for bipropellant combinations.	
Table 3: Critical properties of oxygen and hydrogen.	
Table 4: Theoretical mode frequencies for basic chamber dimensions of BKH.	72
Table 5: BKH injector design parameters.	73
Table 6: FE calculated mode frequencies for BKH with and without secondary nozzle installed	
Table 7: Summary of measured acoustic pressure amplitudes for various BKH configurations and excitation conditions	.119
Table 8: Injection parameters for studies of flame response.	.131
Table 9: Injection parameters for tests with shadowgraph imaging	.155
Table 10: Gas properties and correlating ratios for three different types of atmospheres surrounding LOx droplets in	1 the
reacting coaxial spray	.172

Glossary

Nomenclature

Α	Area	LOx	Liquid oxygen
β*	Reduced acoustic admittance	ṁ	Mass flow rate
С	Sound speed	М	Molecular mass, g/mol
c*	Characteristic exhaust velocity	M_{bulk}	Bulk flow Mach number
Cp	Specific heat capacity	n	Mode index
CH ₄	Methane	N	Response factor
D	Diameter	N_2	Nitrogen
η_{c^*}	Characteristic exhaust velocity efficiency	O ₂	Oxygen
f	Frequency	p	Pressure
F	Thrust	p'	Acoustic pressure
g 0	Standard gravitational acceleration, 9.8 m/s ²	Pcc	Combustion chamber pressure
GH_2	Gaseous hydrogen	ġ	Heat release rate
GN_2	Gaseous nitrogen	ρ	Density
GOx	Gaseous oxygen	R_p	Rayleigh index based on acoustic pressure
γ	Ratio of specific heats	Ru	Rayleigh index based on acoustic velocity
H ₂	Hydrogen	ROF	Oxidiser-to-fuel mixture ratio
1	OH* emission intensity	t	Time
I _{sp}	Specific impulse	T	Temperature
J	Momentum flux ratio	и	Velocity
L	Length	u'	Acoustic particle velocity
LH ₂	Cryogenic ('liquid') hydrogen	VR	Inner-to-outer-propellant injection velocity ratio
LN ₂	Liquid nitrogen		
-112	Eldara Illa ogoti		

Subscripts

y-axis direction

z-axis direction

у

Z

CFD Computational Fluid Dynamics bulk Bulk, total combustion chamber CNRS СС National Scientific Research Centre (France) Critical therophysical property crit DLR German Aerospace Center Droplet (of LOx) d FEA Finite Element Analysis Hydrogen (fuel) Н **IRPHE** Research Institute for Equilibrium Systems (France) Main (exhaust) nozzle MN ONERA National Aerospace Lab (France) 0 Oxygen (oxidiser) NASA National Aeronautics and Space Administration SN Secondary (exhaust) nozzle χ x-axis direction

Acronyms

Abstract

Self-sustaining pressure oscillations in the combustion chamber, or combustion instability, is a commonly encountered and potentially damaging phenomenon in liquid propellant rocket engines (LPREs). In the high-frequency variety of combustion instability, the pressure oscillations in the combustion chamber take on the form and frequency of an acoustic resonance mode of the combustion chamber volume. The most common mode in naturally occurring instability, and also the most destructive, is the first tangential mode, with acoustic gas oscillations oriented transversally to the direction of propellant injection. The instability is driven by the coupling between acoustic oscillations and unsteady energy release from combustion. The mechanisms through which injection and combustion firstly respond to the acoustic field, and secondly feed energy back into the acoustic field have not yet been fully characterised.

Shear coaxial-type injectors are common in LPREs. Past experimental and numerical research efforts have investigated the interaction between this type of injector and transverse acoustic fields. Some experimental efforts have successfully forced transverse acoustic modes and studied their influence on shear coaxial injection under LPRE-like conditions. Acoustic forcing of coaxially injected LOx/H₂ has previously been conducted only at low pressures and injection performance levels. This work addresses the lack of experimental data available for the interaction of shear coaxial injection of LOx/H₂ with acoustics under conditions representative of industrial engines.

A new experimental rocket combustor, designated 'BKH', was developed for investigating the response of a reacting spray of coaxially injected LOx/H₂ to an acoustic field. For characterising the response, simultaneous high-speed recordings of both backlit shadowgraph and hydroxyl radical (OH*) chemiluminescence imaging have been captured through optical access windows. The operating conditions of BKH extend to conditions more representative of actual LPREs than has previously been achieved with LOx/H₂ in studies of flame-acoustic interaction. BKH was run at pressures of 40 or 60 bar, which correspond to subcritical and supercritical thermo-physical regimes for oxygen. Hydrogen injection temperature was ambient, around 290 K, or cryogenic, around 50 K. An array of multiple injectors was used to better represent real engines. A system for modulating the nozzle exhaust flow was used to induce acoustic perturbations inside the combustion chamber. Two types of perturbation were applied to the near-injection region; oscillating acoustic pressure, and oscillating transverse acoustic velocity.

BKH was used to investigate how subcritical or supercritical pressure level and ambient or cryogenic hydrogen injection temperature influence the interaction of acoustic pressure or velocity with injection and combustion processes. Shadowgraph imaging reveals up to 70% reduction in the length of the oxygen jet when subjected to acoustic velocity of amplitude approaching that of the hydrogen injection velocity. Furthermore, the mode of jet breakup changes from its natural growth-and-detachment behaviour to a 'transverse stripping' mechanism. OH* imaging reveals a corresponding decrease in the extent of the flame, and increase in emission intensity. When subjected to acoustic pressure, OH* emission from the flame was observed to fluctuate in phase with pressure. Thus, responses to both acoustic pressure and velocity have been observed in BKH, which together may form the basis of a coupling mechanism for driving natural combustion instability in LPREs.

Declaration of originality

I certify that this work contains no material which has been accepted for the award of any other degree or diploma in any university or other tertiary institution and, to the best of my knowledge and belief, contains no material previously published or written by another person, except where due reference has been made in the text. In addition, I certify that no part of this work will, in the future, be used in a submission for any other degree or diploma in any university or other tertiary institution without the prior approval of the University of Adelaide and where applicable, any partner institution responsible for the joint-award of this degree.

I give consent to this copy of my thesis, when deposited in the University Library, being made available for loan and photocopying, subject to the provisions of the Copyright Act 1968.

I also give permission for the digital version of my thesis to be made available on the web, via the University's digital research repository, the Library catalogue and also through web search engines, unless permission has been granted by the University to restrict access for a period of time.

Justin S. Hardi

June 2012

Acknowledgements and disclaimer

First and foremost I would like to thank my supervisors, A/Prof Bassam Dally and Prof Michael Oschwald. Their guidance was invaluable, and their expertise and patience were an endless source of inspiration. A special mention must also be made of Dr Gerald Schneider who made it possible for me to leave little old Adelaide for the exciting world of aerospace in Europe.

I am indebted to Dimitry Suslov and Bernhard Knapp for their additional valued guidance.

For their collaboration in development of the BKH combustor, I would like to thank Gerhard Krühsel and the Engineering department, especially David Hladik. Thanks also to all personnel of the M10 and M29 workshops, to M3 technicians Michael Zepmeisel and Markus Dengler, and to Andreas Märklen for their expertise in hardware preparation. Philipp Groß and the P8 Test Facility team are acknowledged for their professional efforts in test operations. Thanks to Walter Clauß for the design and operation of optical diagnostics.

I wish to express my gratitude to my fellow students who assisted me over the course of the project; Samuel Webster, Scott Beinke, Harvey Camilo Gomez Martinez, Jannis Schücker, Maike Neuland and Filip Dimoski. I hope you learned as much from me as I did from all of you.

To my colleagues and good friends Michele Negri, Stefan Gröning, and all the Wohnheimers who made coming to work so enjoyable, as well as life in Möckmühl, cheers!

Finally, I owe my deepest gratitude to my family and to Katharina Wirth for their love and support.

Research undertaken for this report has been assisted with a grant from the Smith Fund (www.smithfund.org.au). The support is acknowledged and greatly appreciated.

The Smith Fund by providing funding for this project does not verify the accuracy of any findings or any representations contained in it. Any reliance on the findings in any written report or information provided to you should be based solely on your own assessment and conclusions. The Smith Fund does not accept any responsibility or liability from any person, company or entity that may have relied on any written report or representations contained in this report if that person, company or entity suffers any loss (financial or otherwise) as a result.

